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ISHIO HIDEKI
MIKI TETSUYA

(54) SPECTROMETER

(57)Abstract:
PURPOSE: To make it possible to analyze and combine lights of multiple wavelengthes without any close control by arranging a plurality of filters, which have different transmission wave bands, thereby to accomplish the analysis and combination of the multiple wavelengthes.
CONSTITUTION: Optical signal waves composed of different wavelengthes $\lambda 1$, $\lambda 2$, $\lambda 3$, $\lambda 4$ and $\lambda 5$ are emitted from a fiber 100 and converted by a colimating lens 40 into parallel beams, which enter an optical filter 11. In accordance with the characteristics of the filter 11, the signal waves of the wavelength $\lambda 1$ are allowed to pass through the filter 11 and are gathered in a photoelectric converting element 31 by a condensing lens 21 so that the signal waves of other wavelengthes are reflected to enter an optical filter 12. The signal waves of the wavelength $\lambda 2$ are allowed to pass through the filer 12 whereas the others are reflected to enter an optical filter 13. Likewise, sequential separations are accomplished so that the signal wavelengthes of the wavelengthes $\lambda 2$, $\lambda 3$ and so on are sequentially gathered at other photoelectric converting elements 32, 33 and so on. In the case of spectroscopy, the characteristics of the respective filters can be independently adjusted, and the size can slso be reduced with ease.

LEGAL STATUS

[Date of request for examination]

[Date of sending the examiner's decision of rejection]

[Kind of final disposal of application other than the examiner's decision of rejection or application converted registration]

[Date of final disposal for application]

[Patent number]

[Date of registration]

[Number of appeal against examiner's decision of rejection]

[Date of requesting appeal against examiner's decision of rejection]

[Date of extinction of right]

Ref. ②

⑲日本国特許庁(JP)

⑪特許出願公開

⑫公開特許公報(A)

昭54—103055

⑤Int. Cl.²　G 02 B 5/14　G 02 B 27/10

識別記号

㊗日本分類　104 A 0　104 G 0

庁内整理番号　7244—2H　7448—2H

㊸公開　昭和54年(1979) 8月14日

発明の数 1

審査請求 未請求

(全 4 頁)

㊿光分波器

㉑特　　願　昭53—8873

㉒出　　願　昭53(1978) 1月31日

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⑦出 願 人　日本電信電話公社

⑭代 理 人　弁理士 山本恵一

明　細　書

1. 発明の名称

光分波器

2. 特許請求の範囲

特定の波長の光を透過させ他の波長の光を反射させる少なくとも1個のフィルタと，該フィルタを光を順次反射可能なごとく配置した配列と，第1のフィルタに光ビームを斜めに入射させる手段と，各フィルタの透過光を受容する手段とを有し，各フィルタの透過波長がフィルタ毎に相互に異なることを特徴とする光分波器。

3. 発明の詳細な説明

本発明は，光学機器における分光或いは，複数の波長の光信号を多重伝送する波長分割多重伝送方式における光信号の結合又は，分離などに用いる光分波器に関するものである。

従来，干渉膜フィルタを利用した光分波器の一形式として，内部干渉膜を有する集束性ロッドレンズがあった。これは，第1図に示すように，二つの集束性ロッドレンズ1，2の間に，干渉膜3をはさんだ構造になっている。集束性ロッドレンズ1，2は，レンズ作用を持ち，レンズ内に入射した光は，集束性ロッドレンズ内を蛇行して進む。分波器として用いる場合，集束性ロッドレンズ1，2の長さは，光ビームの蛇行ピッチの約1／4に選ばれる。干渉膜3は，誘電体多層膜による波長依存性反射膜で，反射率及び透過率が光の波長で異なる。

光ファイバ100に異なる二つの波長λ_1，λ_2の信号が導かれ，これを異なる位置に分波する場合を説明する。ファイバ100から出射した二つの異なる波長の光信号波は蛇行しながら，集束性ロッドレンズ1内を伝搬し，干渉膜3に入射する。干渉膜3は，波長λ_1の光信号波を反射し，波長λ_2の光信号波を透過する。波長λ_1の光信号波は，反射されて光ファイバ101に入射する。波長λ_2の光信号波は，集束性ロッドレンズ2内を伝搬し，光ファイバ102に入射する。したがって，波長の異なる二つの光信号波を分離できる。干渉膜3の分波特性は，ファイバ100の位置5で決まる。分波され

た信号波を受けるファイバ101，102 の位置6，7もファイバ100の位置5で決まる。従って，干渉膜3の分波特性と，受信用ファイバ101，102の位置を独立に調整することはできない。

三つ以上の，波を分離する場合第2図に示したように，集束性ロッドレンズ1，2，1′，2′，1″，2″を組み合せた構造になるが，集束性ロッドレンズ1，2，1′，2′，1″，2″の接続位置を精密に制御しないと，損失は増大する。分波しなければならない信号波の数が増大する程，その困難さも増大する。

従って本発明は従来の技術の上記欠点を改善するもので，その目的は精密な制御なしに多数の波長の光を分波又は結合することの出来る光分波器を提供することにあり，その特徴は，フィルター列により多数の波長の信号波の分離もしくは多重を行なう光分波器にある。以下図面により詳細に説明する。

第3図は，本発明の分波器10の実施例である。11，12，13，14，15は干渉膜フィルタ，21，22，23，24，25は集光用レンズ，31，32，33，34，35は光電変換素子，40は，コリメートレンズである。光フィルタ11，13，15から成るフィルタ列は，光フィルタ12，14から成るフィルタ列に対して平行に並んでいるものとする。光フィルタ11は，分波される光信号波の内で，波長λ_1の光信号波のみを透過し，他は反射する。光フィルタ12は分波される光信号波の内で，波長λ_2の光信号波のみを透過する。以下同様に光フィルタ13，14，15は，各々，波長λ_3，λ_4，λ_5の光信号波のみを透過する。本発明は，このように通過波長帯が異なる複数個のフィルタを列状に並べて多数の波長の分波及び合波を行なうものである。以下に本分波器の動作原理を説明する。

いま，異なる波長λ_1，λ_2，λ_3，λ_4，λ_5から成る光信号波が，ファイバ100から出射され，コリメートレンズ40で平行ビームに直され，光フィルタ11に入射するとする。光フィルタ11の特性から，波長λ_1の光信号波は光フィルタ11を透過し，他の波長の光信号波は，反射され光フィルタ12に入射する。光フィルタ11を透過した波長λ_1の光信号波は，集光レンズ21で光電変換素子31に集められる。一方光フィルタ12に入射した光ビームうちで，波長λ_2の光信号波のみ透過し，集光レンズ22で，光電変換素子32に集められ，他の波長の光信号波は反射されて，光フィルタ13に入射する。以下同様にして光フィルタにより順次光信号波が分離される。図3の例では，フィルタが5個であったが，更に通過波長域が異なるフィルタを並べることにより，更に多くの光信号波を分波できることは，もちろんである。

第4図は光合波器10の例を示している。信号光源31′，32′，33′，34′，35′は，各々，波長λ_1，λ_2，λ_3，λ_4，λ_5の信号光源であり，コリメートレンズ21′，22′，23′，24′，25′は，信号光源の光を平行ビームにするコリメートレンズであり，集光レンズ40′は，各波長の光信号波をファイバ100に結合させる。この場合，波長λ_1の光信号波は光フィルタ11を通過し，集光レンズ40′で集められ，ファイバ100に導入される，波長λ_2の光信号波は光フィルタ12を通過し，光フィルタ11で反射し，集光レンズ40′で集められ，ファイバ100に導入される，以下同様にして，波長λ_3，λ_4，λ_5の光はファイバ100に結合される。

第5図は，個々のフィルタを一直線上に並べないで，角度を付けて並べたもので，分波合波が，第3図及び第4図の例と同様に行なう事が出来る。

以上説明したように，本発明によれば波長が異なる多数の光信号を合波したり分離する分波器を構成する際；

(1) 個々のフィルタ特性を独立に調整できる。すなわち，分波する場合，フィルタへの光信号波の入射角と受信用光電変換素子（合波の場合は信号光源）の位置を独立に調整できる。

(2) 小形化が容易である。

(3) 集束性ロッドレンズを用いた光分波器よりも，個々の部品の精度，部品間の位置精度に対する許容度が大きい。

という利点がある。

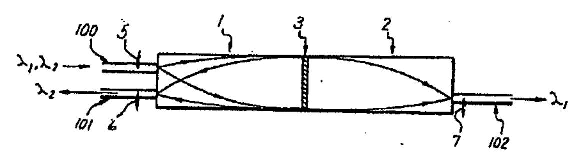
4. 図面の簡単な説明

第1図は，従来の集束形ロッドレンズを用いた二波用分波器の構成図，第2図は，従来の集束形ロッドレンズを用いた四波用分波器の構成図，第3図は，本発明の分波器の一実施例，第4図は本発明の合波器の一実施例，第5図は本発明の分波器の別の構造例である。

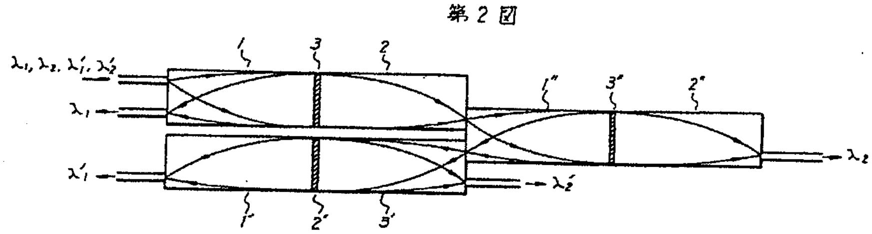
1，1′，1″，2，2′，2″……集束形ロッドレンズ，3，3′，3″……干渉膜フィルタ，5……光ファイバ100の位置，6……光ファイバ101の位置，7……光ファイバ102の位置，100，101，102……光ファイバ，11，12，13，14，15……光フィルタ，21，22，23，24，25……集光用レンズ，21′，22′，23′，24′，25′……コリメートレンズ，31，32，33，34，35……光電変換素子，31′，32′，33′，34′，35′……信号光源，40……コリメートレンズ，40′……集光レンズ，100……光ファイバ。

特許出願人　日本電信電話公社
特許出願代理人　弁理士　山本恵一

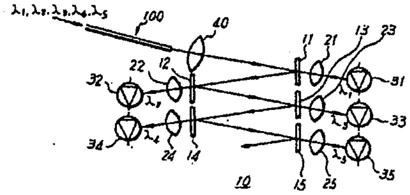
第1図



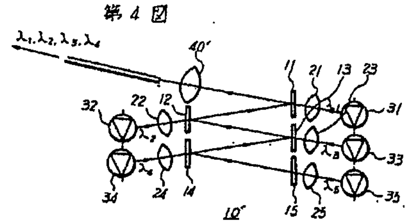
第2図



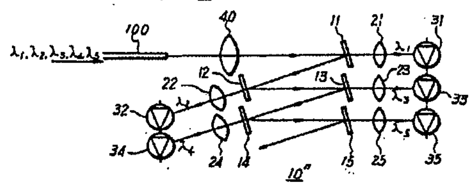
第3図


λ1,λ2,λ3,λ4,λ5
100
40
11
21
13
23
22
12
32
31
33
34
24
14
10
15
25
35

第4図


λ1,λ2,λ3,λ4
40'
11
21
13
23
32
22
12
31
33
34
24
14
10'
15
25
35

第5図


λ1,λ2,λ3,λ4,λ5
100
40
11
21
31
22
12
13
23
33
32
34
24
14
10''
15
25
35

Corresponding to Ref. ②

17p.

United States Patent [19]

Nosu et al.

[11] 4,244,045

[45] Jan. 6, 1981

[54] OPTICAL MULTIPLEXER AND DEMULTIPLEXER

[75] Inventors: Kiyoshi Nosu, Yokohama; Hideki Ishio; Tetsuya Miki, both of Yokosuka, all of Japan

[73] Assignee: Nippon Telegraph and Telephone Public Corporation, Tokyo, Japan

[21] Appl. No.: 8,161

[22] Filed: Jan. 31, 1979

[30] Foreign Application Priority Data

Jan. 31, 1978 [JP] Japan 53/8873

[51] Int. Cl.³ H04B 9/00

[52] U.S. Cl. 370/3; 455/612; 455/617

[58] Field of Search 250/199; 358/50; 350/172; 370/3; 455/612, 617

[56] References Cited

U.S. PATENT DOCUMENTS

3,403,260 9/1968 Geusic 350/172

3,623,797 11/1971 Daw 350/172

3,703,640 11/1972 Broussaud 250/199

3,953,727 4/1976 d'Auria 250/199

4,001,577 1/1977 Albanese 250/199

Primary Examiner—Howard W. Britton

Attorney, Agent, or Firm—Armstrong, Nikaido, Marmelstein & Kubovcik

[57] ABSTRACT

An optical multiplexer and/or optical demultiplexer for multiplexing and/or demultiplexing a plurality of wavelengths comprises a plurality of optical filters each of which transmits a predetermined wavelength and reflects other wavelengths, said optical filters being arranged so that an optical beam is transmitted or reflected via each optical filter in sequence in a zigzag fashion. A light source or light detector is provided behind each optical filter to project or receive a collimated optical beam. The angle of incidence when a beam is applied to an optical filter is small. And, another optical means is provided to connect the present optical multiplexer and/or demultiplexer with an outside optical fiber. The transmission wavelength of each optical filter is different from the others.

20 Claims, 17 Drawing Figures

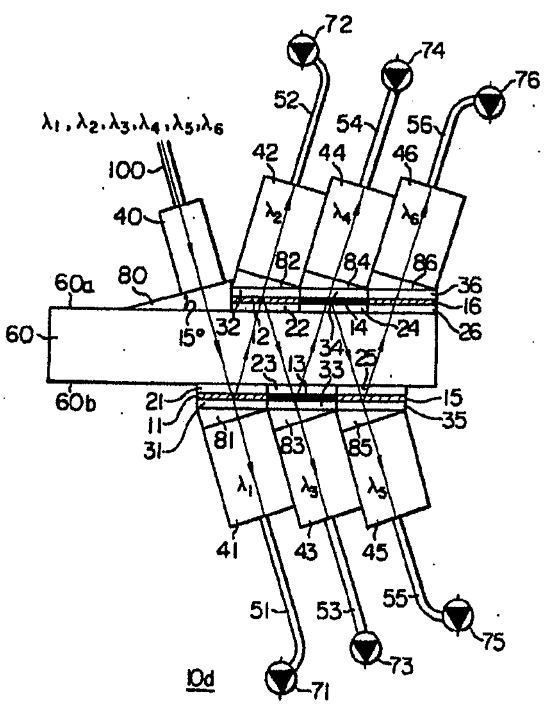
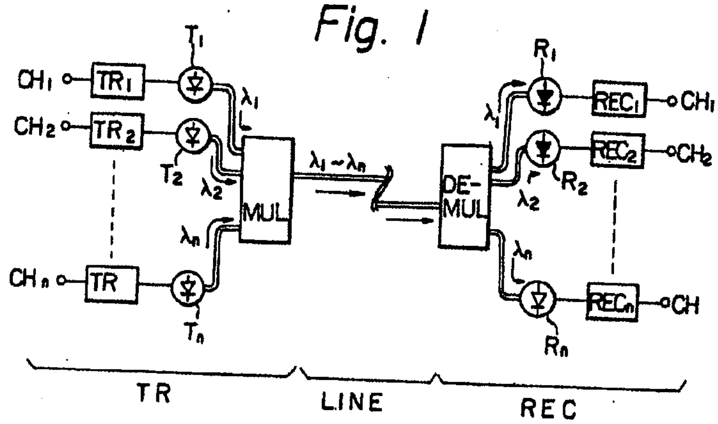
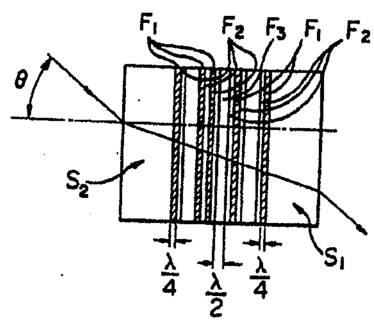


Fig. 1



CH1
TR1
T1
λ1
CH2
TR2
T2
λ2
CHn
TR
Tn
λn
MUL
λ1~λn
DE-MUL
R1
REC1
CH1
R2
REC2
CH2
λ2
λn
Rn
RECn
CH
TR
LINE
REC

Fig. 4



F1
F2
F3
F1
F2
θ
S2
S1
λ/4
λ/2
λ/4

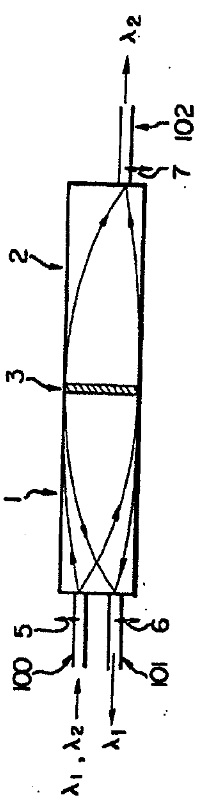


Fig. 2

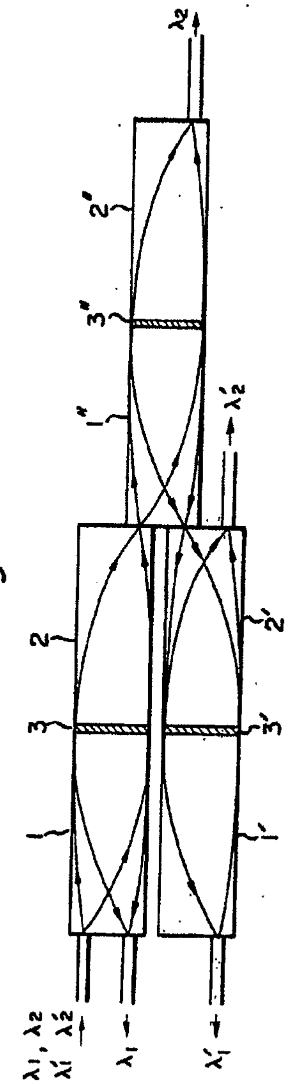


Fig. 3

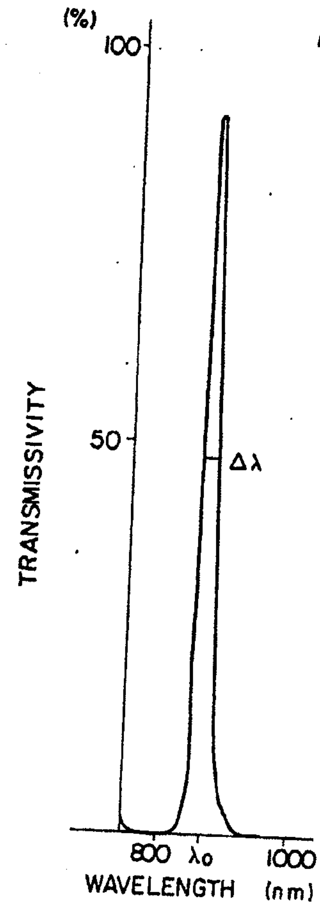


Fig. 5

Fig. 6

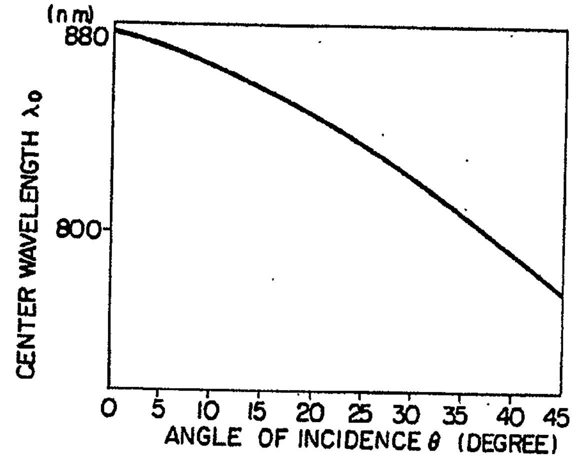


Fig. 7

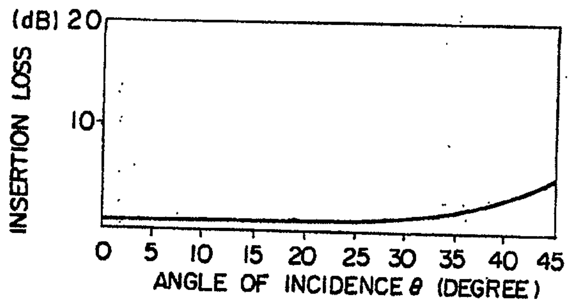


Fig. 8

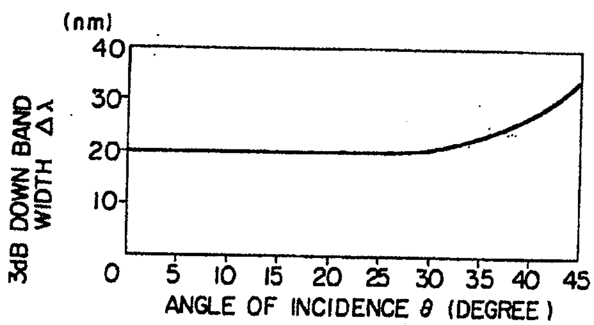


Fig. 9

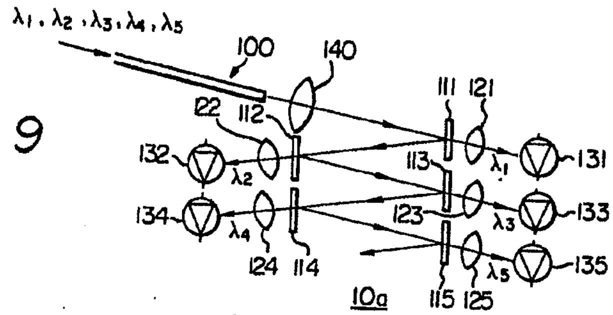


Fig. 10

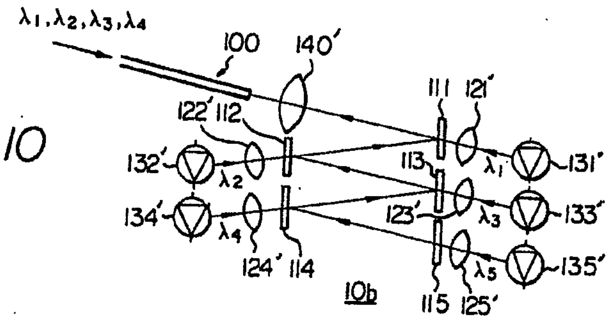


Fig. 11

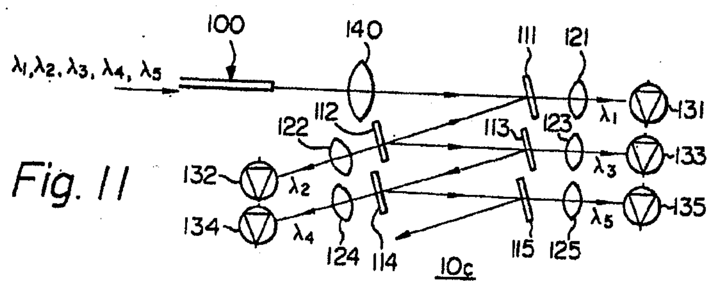


Fig. 12

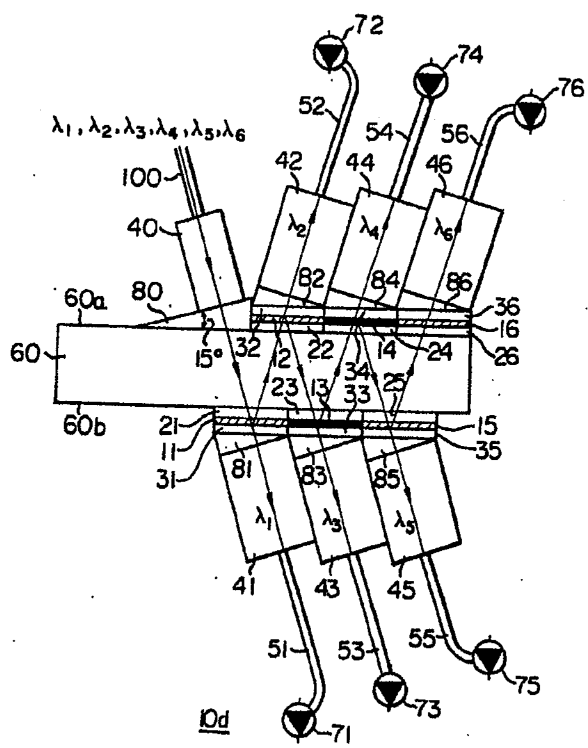

72
74
76
52
54
56
$\lambda_1, \lambda_2, \lambda_3, \lambda_4, \lambda_5, \lambda_6$
100
42
44
46
40
λ_2
λ_4
λ_6
82
84
86
60a
80
36
16
60
15°
32
12
22
14
24
26
23
13
34
33
25
60b
21
11
31
15
35
81
83
85
λ_1
λ_3
λ_5
41
43
45
51
53
55
75
73
10d
71

Fig. 13

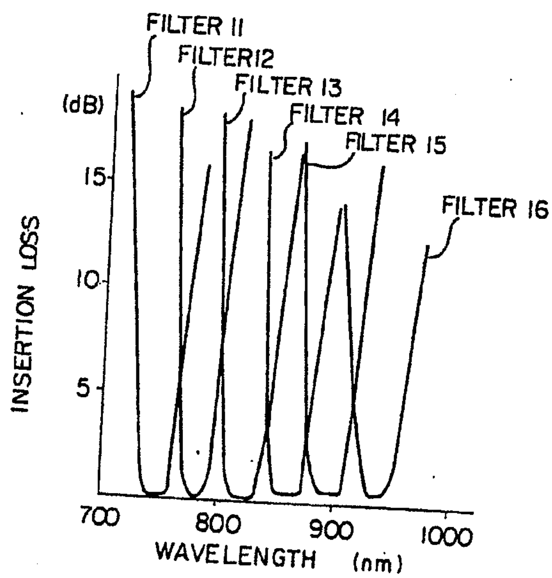

FILTER 11
FILTER12
FILTER 13
FILTER 14
FILTER 15
FILTER 16
(dB)
15
10
5
INSERTION LOSS
700
800
900
1000
WAVELENGTH (nm)

Fig. 14

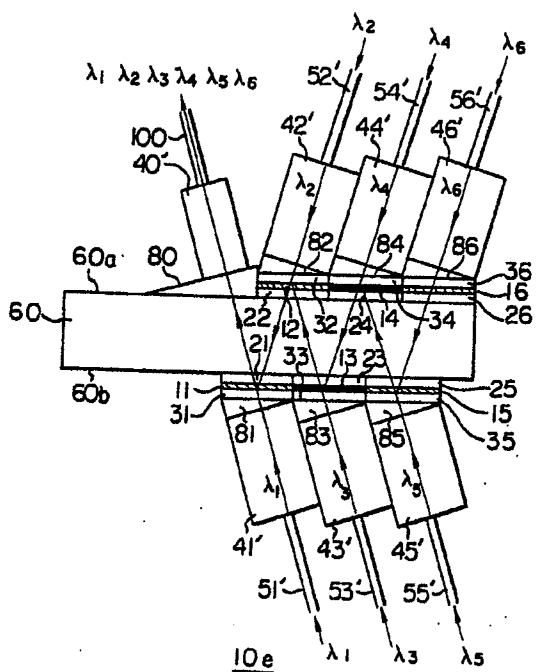


Fig. 15

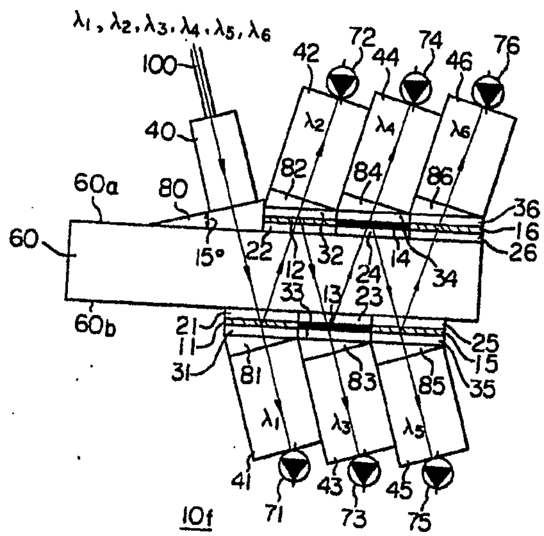

λ1, λ2, λ3, λ4, λ5, λ6
100
40
42
72
44
74
46
76
λ2
λ4
λ6
82
84
86
60a
80
36
16
26
60
15°
22
12
32
14
34
33
13
24
23
60b
21
11
31
81
83
85
25
15
35
λ1
λ3
λ5
41
43
45
71
73
75
10f

Fig. 16

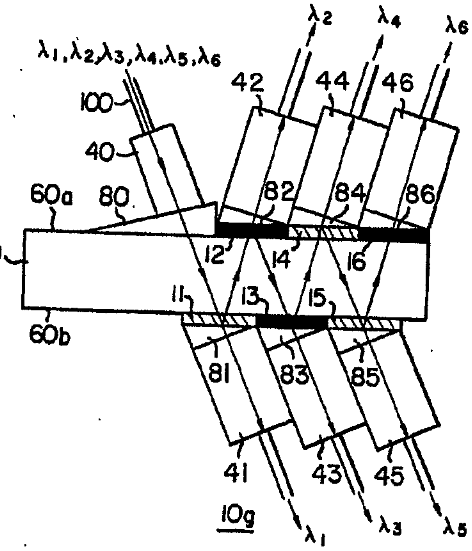
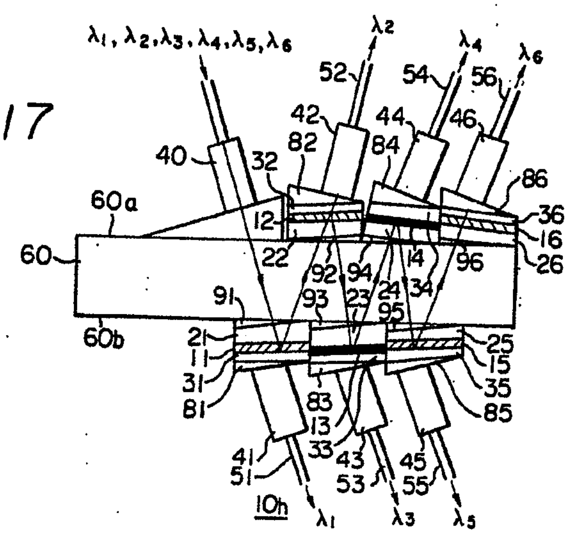

λ1, λ2, λ3, λ4, λ5, λ6
λ2
λ4
λ6
100
40
42
44
46
60a
80
82
84
86
60
12
14
16
11
13
15
60b
81
83
85
41
43
45
10g
λ1
λ3
λ5

Fig. 17


λ1, λ2, λ3, λ4, λ5, λ6
λ2
λ4
λ6
52
54
56
42
44
46
40
32
82
84
86
60a
12
36
16
60
22
92
94
14
96
26
91
93
23
24
34
95
60b
21
11
31
81
25
15
35
85
83
13
33
43
45
41
51
53
55
10h
λ1
λ3
λ5

OPTICAL MULTIPLEXER AND DEMULTIPLEXER

BACKGROUND OF THE INVENTION

The present invention relates to an optical multiplexer and/or an optical demultiplexer which can be utilized for spectroscopic analysis in optical equipment, and/or combining and/or separation of optical signals in wavelength-division multiplexing transmission system.

A telecommunication system utilizing an optical fiber transmission system has the advantages over prior metallic cables, such as small loss, wide bandwidth, small cable diameter, light-weight cable, high-flexibility cable, no cross talk characteristic, and immunity to electromagnetic interference. And the latest developments for manufacturing optical fiber with low loss, and for controlling the wavelength in light sources, makes possible a wavelength-division multiplexing transmission system which transmits a plurality of wavelengths in a single optical fiber. This technology not only increases the transmission capacity of an optical fiber, but also makes possible a two-way transmission system and/or simultaneous transmission of a plurality of different signals.

FIG. 1 shows an example of the basic configuration of a wavelength-division multiplexing transmission system (called W.D.M.). In this figure, the signals of a plurality of channels ($CH_1, CH_2, \ldots, CH_n$) at the transmission side are converted to a driving signals for driving light sources by respective transmitter circuits ($TR_1, TR_2, \ldots, TR_n$), and are applied to light sources ($T_1, T_2, \ldots, T_n$). Each light source generates a light beam according to said driving signals and each of said light beams has the center wavelength ($\lambda_1, \lambda_2, \ldots, \lambda_n$), and each of said center wavelengths corresponds to a different channel. As a light source a laster or a light-emitting-diode (LED) can be generally utilized. The output light beams from the light sources are applied to an optical multiplexer (MUL) through an optical fiber and are multiplexed or combined therein, then the multiplexed light beams are applied to an optical fiber transmission line (LINE).

At the reception side, each wavelength is separated from the others by an optical demultiplexer (DEMUL), and each separated light beam is applied to each light detector or sensor ($R_1, R_2, \ldots, R_n$), which converts the optical signal to an electrical signal. Said electrical signal is applied to a corresponding output terminal through a receiver circuit ($REC_1, REC_2, \ldots, REC_n$).

It should be appreciated that, in a two-way WDM transmission system, both the light sources and the light detectors are provided at both the transmission side and the reception side.

The present invention provides an optical multiplexer and/or an optical demultiplexer utilized as mentioned above as an example. It should be noted that due to the reversibility of a light beam, the structure of an optical multiplexer is the same as the structure of an optical demultiplexer. Accordingly, it should be noted that the word "multiplexer" or "demultiplexer" involves both a multiplexer and a demultiplexer unless a specific definition is given.

Some of the prior devices which can be utilized as an optical multiplexer are a prism, an optical grating, and a wavelength-selective filter. A prism and an optical grat-

ing are wavelength selective devices which utilize the relationship between the wavelength and the refractive index, or diffraction angle of a prism or an optical grating, respectively.

A wavelength selective filter reflects a specific wavelength and transmits other wavelengths, and is embodied by plastics with coloring matter or dye, or a laminated thin film interference filter in which thin film multi-layers are attached on a glass substrate through vacuum evaporation.

A graded index rod lens has a radial index profile of the refractive index as shown below.

$$N(r)=N_0(1-(A^2/2)r^2)$$

where N(r) is the refractive index at the point of the radius (r), N_0 is the center refractive index, A is a constant, and r is the length from the center. When a light beam is applied to the center of the rod in the axial direction, the diameter of the beam changes periodically, and when a light beam is applied to a portion other than the center of the rod, the light beam goes in a zigzag fashion. The combination of the above characteristics of a rod lens and an interference thin film filter provides an optical multiplexer.

This optical multiplexer has a structure as shown in FIG. 2, in which an interference filter 3 is sandwiched between a pair of graded index rod lenses 1 and 2. The light beam coming into the graded index rod lens proceeds in a zigzag fashion through the graded index rod lens as shown by the arrow in the figure. When used as an optical multiplexer, the lengths of the graded index rod lenses 1 and 2 are designed to be about ¼ of the zigzag pitch of the light beam. The interference thin film filter 3 is a reflection film made of dielectric multi-layer film with a wavelength dependency characteristic, that is, reflectivity and transmissivity of this film differs depending on the wavelength of the light

The following is a description of signals with two different wavelengths λ_1, and λ_2, introduced into the optical fiber 100, and separated into two different positions. The optical signal waves of two different wavelengths emitted from the optical fiber 100 proceed zigzag and propagate through the graded index rod lens 1 and enter the interference filter 3. Then, the interference filter 3 reflects the optical signal wave with wavelength λ_1 but transmits the optical signal wave with wavelength λ_2. The optical signal wave with wavelength λ_1 is reflected and enters the optical fiber 101. The optical signal wave with wavelength λ_2 propagates through the graded index rod lens 2 and is introduced into the optical fiber 102. Therefore, the two optical signal waves with different wavelengths can be separated. The characteristics of the interference filter 3 as a multiplexer are determined by the position 5 of the fiber 100. The positions 6 and 7 of the optical fibers 101 and 102 which receive the separated signal waves are also determined by the position 5 of the optical fiber 100. Therefore, the optical multiplexer as shown in FIG. 2 has the disadvantage that the characteristics of the interference filter 3 and the positions of the fibers 101 and 102 for reception of the waves cannot be adjusted independently.

When three or more waves are to be separated, the configuration shown in FIG. 3 is utilized. In this case, a plurality of graded index rod lenses 1, 2, 1', 2', 1'', 2'' are assembled. However, loss will be great if connecting

positions of these graded index rod lenses are not controlled with precision. The larger the number of signal waves to be separated, the greater the adjustment difficulties.

Another prior optical multiplexer utilizing a wavelength selective mirror is disclosed in the U.S. Pat. No. 3,953,727. According to said U.S. patent, a plurality of selective mirrors oriented at 45 degrees in relation to the axis of the light beam are arranged in a cascaded configuration, and each selective mirror reflects a specific wavelength. Accordingly, when there are many wavelengths to be multiplexed or demultiplexed, a light beam must pass many selective filters, therefore, the transmission loss is great. Further, said U.S. patent has the disadvantage that when the wavelength to be separated is near to that of the other wavelength, separation is impossible since the angle of incidence is as large as 45 degrees, and the transmission and/or reflection characteristics of that filter depends upon whether the light beam is P-polarized light or S-polarized light.

Said U.S. patent also discloses a multiplexer in which a plurality of band pass filters are arranged around a glass plate with semi-reflective walls. However, this multiplexer has the disadvantage that the loss of the light beam is great since the light beam suffers from a plurality of partial reflections or partial transmission in said semi-reflective walls.

SUMMARY OF THE INVENTION

It is an object, therefore, of the present invention to overcome the disadvantages and limitations of prior multiplexer and/or demultiplexer by providing a new and improved optical-multiplexer and/or demultiplexer.

It is also an object of the present invention to provide a multiplexer and/or demultiplexer in which the insertion loss is small, the angle of incidence is small, and many signals can be multiplexed.

The above and other objects are attained by an optical multiplexer and demultiplexer comprising at least one optical filter which transmits a predetermined wavelength and reflects other wavelengths, said optical filter being arranged so that an optical beam is transmitted or reflected by said optical filter in sequence in a zigzag fashion, means for projecting or receiving a collimated optical beam to or from the first optical filter with a small angle of incidence, a light source or a light detector positioned behind each optical filter, means for connecting the output of the final optical filter to an external optical fiber, and the transmission wavelength depending upon each specific optical filter.

BRIEF DESCRIPTION OF THE DRAWINGS

The foregoing and other objects, features, and attendant advantages of the present invention will be appreciated as the same become better understood by means of the following description and accompanying drawings wherein;

FIG. 1 shows the general view of a wavelength division multiplex communication system utilizing the present invention,

FIG. 2 shows the structure of a prior optical multiplexer,

FIG. 3 shows the structure of another prior optical multiplexer,

FIG. 4 shows the structure of a dielectric thin film filter utilized in the present invention,

FIG. 5 shows the relationship between the wavelength and the transmissivity of the filter in FIG. 4,

FIG. 6 shows the curve between the center wavelength of the filter and the angle of incidence of the filter in FIG. 4,

FIG. 7 shows the curve between the angle of incidence and the insertion loss at the center wave-length of the filter in FIG. 4,

FIG. 8 shows the relationship between the angle of incidence and the 3-dB down wavelength width (that is, the half width) of the filter in FIG. 4,

FIG. 9 is the basic configuration of the present optical demultiplexer,

FIG. 10 is the basic configuration of the optical multiplexer according to the present invention,

FIG. 11 is another configuration of the present optical demultiplexer,

FIG. 12 shows the detailed structure of the present optical demultiplexer,

FIG. 13 shows the characteristics of the demultiplexer shown in FIG. 12,

FIG. 14 shows the detailed structure of the present optical multiplexer,

FIG. 15 shows the detailed structure of another embodiment of the present optical demultiplexer,

FIG. 16 shows the detailed structure of still another embodiment of the present optical demultiplexer, and

FIG. 17 shows the detailed structure of still another embodiment of the present optical demultiplexer.

DESCRIPTION OF THE PREFERRED EMBODIMENTS

FIG. 4 shows the embodiment of the structure of the dielectric thin film filter, which has a laminated structure, comprising a plurality of the first laminated layers with F_1 and F_2, the second signal layer with F_3 and the third laminated layers with F_1 and F_2. The layer F_1 is made of Z_nS and has the thickness $\lambda/4$, the layer F_2 is made of M_gF_2 and has the thickness $\lambda/4$, and the layer F_3 is made of Z_nS and has the thickness $\lambda/2$. Preferably, the first laminated layer with F_1 and F_2 has about ten F_1 layers and the same number of F_2 layers alternatively, and the third laminated layers with F_1 and F_2 have the same structure as the first layers. Preferably, those layers are attached to a glass substrate S_1, and the surface of the layers is covered with a protection layer or cover glass S_2. The dielectric thin film filter mentioned above provides the bandpass characteristic in which the specified wavelength λ among the input light beam transmits, and another wavelengths are reflected. The adjustment of the thickness of the layers F_1, F_2 and F_3 can control the passband of the filter as desired. Further, when a light beam is applied to a filter obliquely with some angle $\theta(\theta \neq 0)$ of incidence, the pass-band (or a center wavelength) of a filter is determined according to the thickness of the layers in the direction of the light beam. Therefore, the passband for an oblique light beam is different from that for a perpendicular light beam. It should be noted in the explanation hereinafter that the present multiplexer has the feature that the angle of incidence is small.

FIG. 5 illustrates an example of measuring the wavelength characteristics of transmissivity of the dielectric thin film filter having bandpass characteristic in FIG. 4 according to the present invention. In FIG. 5, the horizontal axis indicates wavelength and the vertical axis transmissivity. In this example, the center wavelength λ_0 is 875 nm, and the half width $\Delta\lambda$ is 20 nm. The half

width $\Delta\lambda$ is the wavelength width in which the energy decreases by 3dB compared with the center wavelength. Of course the wavelengths which do not transmit are reflected.

FIG. 6 illustrates an example of the relationship between the center wavelength λ_0 of the bandpass filter and the angle of incidence of a light beam. As apparent from FIG. 6, the larger the angle of incidence θ, the more the center wavelength λ_0 shifts to the shorter wavelength side.

FIG. 7 illustrates an example of the relationship between the insertion loss and the angle of incidence θ at the center wavelength λ_0 of the bandpass filter.

FIG. 8 depicts an example of the relationship between the half width $\Delta\lambda$ of the bandpass filter and the angle of incidence.

From these examples, the following can be identified. In FIGS. 6, 7 and 8, when the angle of incidence θ is selected at less than about 20°, the transmissivity T_0 at the center wavelength λ_0 and the half width $\Delta\lambda$ remain the same as those in the case of perpendicular incidence ($\theta=0°$), although only the center wavelength λ_0 is shifted to the shorter wavelength side.

FIG. 9 illustrates an embodiment of the demultiplexer according to the present invention. In FIG. 9, the demultiplexer **10a** comprises a plurality of dielectric thin film filters **111, 112, 113, 114** and **115** the structure of which is shown in FIG. 4, a plurality of condenser lenses **121, 122, 123, 124** and **125**, a plurality of photoelectric conversion elements (light detectors or sensors) **131, 132, 133, 134** and **135**, and a collimating lens **140**. The filter array composed of the optical filters **111, 113** and **115** is to be arranged in parallel with the other filter array composed of the optical filters **112** and **114**. Among the optical signal waves to be demultiplexed, only the optical signal wave with wavelength λ_1 is transmitted through the optical filter **111**, which reflects all other wavelengths. Next, the optical filter **112** transmits only the optical signal wave with wavelength λ_2 and reflects all other wavelengths. In the same manner, the optical filters **113, 114** and **115** transmit optical signal waves with wavelengths λ_1, λ_2, λ_3 respectively. Thus, the present invention separates or combines wavelengths through an array of a plurality of filters with different pass bands.

Now, the operation of the present invention will be described in detail.

Supposing that optical signal waves composed of different wave lengths $\lambda_1, \lambda_2, \lambda_3, \lambda_4, \lambda_5$ are emitted from the optical fiber **100**, and are collimated through the collimator lens **140**, then, the collimated light beam enters the optical filter **111**. According to the characteristics of the optical filter **111**, the optical signal wave with wavelength λ_1 is transmitted through the optical filter **111**, while optical signal waves of other wavelengths are reflected and enter the optical filter **112**, the optical signal wave with wavelength λ_1 which is transmitted through the optical filter **111** is converged by the condenser lens **121** onto the light detector **131**. Similarly, among the light beams that entered into the optical signal wave with wavelength λ_2 transmits through the optical filter **112** and is collimated by the condenser lens **112**, which illuminates the light detector **132**. The optical signal waves with other wavelengths are reflected by the filter **112** and enter the optical filter **113**. Similarly, all other optical signal waves are separated in sequence by the optical filters. Although the embodiment of FIG. 9 consists of five optical filters, by addition of filters of difference transmission wave length bands, many more optical signal waves can of course be filtered.

FIG. 10 shows an embodiment of an optical multiplexer **10b**, in which the signal light sources **131', 132', 133', 134'** and **135'** generate the signals of the wavelengths $\lambda_1, \lambda_2, \lambda_3, \lambda_4, \lambda_5$ respectively. The collimating lenses **121',122', 123' 124'** and **125'** provide parallel light beams relating the corresponding light sources, and the condenser lens **140'** connects the multiplexed optical signals to the optical fiber **100**. In this process, the optical signal wave with wavelength λ_1 passes through the optical filter **111**, collimated by the condenser lens **140'** and is introduced into the optical fiber **100**. The optical signal wave with wavelength λ_2 passes through the optical filter **112**, is reflected by the optical filter **111**, is collimated by the condenser lens **140'**, and is introduced into the optical filter **100**. Similarly, the light beams with wavelengths λ_3, λ_4, and λ_5 are introduced into the optical fiber **100**.

FIG. 11 illustrates a modified configuration of the present demultiplexer **10c** which the optical filters are not arranged on one straight line. Instead, each filter is placed at an angle with reference to the positioning line. With this arrangement, the multiplexing and/or the demultiplexing can be performed in the same manner as the configuration in FIGS. 9 and 10.

FIG. 12 shows the detailed structure of the optical demultiplexer **10d** according to the present invention. In the figure, the reference numerals **11, 12, 13, 14, 15** and **16** are dielectric thin film optical band pass filters, **21, 22, 23, 24, 25** and **26** are glass plates for supporting optical band pass filters **31, 32, 33, 34, 35** and **36** are glass protectors for protecting optical band pass filters, **40** is a graded index rod lens for collimating light from an optical fiber, **41, 42, 43, 44, 45** and **46** are graded index rod lenses for condensing light beams, **51, 52, 53, 54, 55** and **56** are optical fibers for guiding the demultiplexed light to the light detectors or the sensors, **60** is a transparent common substrate having parallel planes **60a** and **60b**, **71, 72, 73, 74, 75** and **76** are light detectors or sensors, **80, 81, 82, 83, 84, 85** and **86** are prisms for coupling the oblique incident light beam to optical filters, and **100** is an optical fiber in a transmission line. It should be appreciated that the vertical angle of the prisms **80** through **86** is the same as the angle of incidence of the optical beams to the optical filters, and said angle is, in the present embodiment, 15 degrees. A series of filters comprising the optical band pass filters **11, 13** and **15** and another series of filters comprising the optical band pass filters **12, 14** and **16** are lined up on both of the parallel surfaces **60a** and **60b** of the common substrate **60**. Further it should be appreciated that the refraction indices of the glass plates **21, 22, 23, 24, 25** and **26**, the glass protections **31, 32, 33, 34, 35** and **36**, graded index rod lenses **40, 41, 42, 43,44,45** and **46**, the common substrate **60**, and the optical fibers **51,52,53,54,55,56** and **100** are approximately equal. Since these components are mutually connected with optical contact and their refraction indices are approximately equal, the reflection at the interface junction of the components is negligibly small. Further, since the center wavelength of the band-pass optical filter **11** is λ_1, a light beam with wavelength λ_1 passes through the band-pass optical filter **11**. However, other wavelengths $\lambda_2, \lambda_3, \lambda_4, \lambda_5, \lambda_6$ which are sufficiently apart from the wavelength λ_1 are reflected by the filter **11**. Similarly the center wavelengths of the optical band-pass fiters **12,13,14** and **15** are $\lambda_2, \lambda_3, \lambda_4, \lambda_5$,

λ_6 respectively and reflect light beams which are apart from the respective center wavelengths. The vertical angle of the prisms 80,81,82,83,84, and 85 is 15° in the present embodiment.

Now the operation of the device in FIG. 12 is described. When light waves with different wavelengths $\lambda_1, \lambda_2, \lambda_3, \lambda_4, \lambda_5, \lambda_6$ are applied to the rod lens 40 from the optical fiber 100, these light waves are collimated to parallel beams and enter the optical band-pass filter 11 with the oblique incidence angle defined by the vertical angle of the prisms 80 through 86. The angle of incidence to the filters in this embodiment is 15°. According to the characteristics of the optical band-pass filter 11, a light wave with the wavelength λ_1 is transmitted through the optical band-pass filter 11. Other waves are reflected by the optical band-pass filter 11 and enter to the second optical band-pass filter 12 through the glass plate 21, the common substrate 60 and the glass plate 22. The wavelength λ_1 which transmits the filter 11, passes through the prism 81, and the rod lens 41, and enters the optical fiber 51, which guides the light wave of the wavelength λ_1 to the sensor 71. Thus, the electrical signal relating to the wavelength λ_1 is obtained at the output of the sensor 71. Next, among the light beams which are reflected by the optical band-pass filter 11 and enter the second optical band-pass filter 12, only the light wave with the wavelength λ_2 is transmitted by the second optical band-pass filter 12, through the prism 82, rod lens 42 and the optical fiber 52 is applied to the sensor 72. Thus, the sensor 72 provides the electrical signal relating the wavelength λ_2 at the output of the sensor 72. The light beams with wavelengths $\lambda_3, \lambda_4, \lambda_5, \lambda_6$ are reflected by the second optical band-pass filter 12 and enter the third optical band-pass filter 13 through the glass plate 22, the common substrate 60 and the glass plate 23. Similarly, the light waves with different wavelengths are separated in sequence through the optical band-pass filters 13, 14, 15 and 16. Although an embodiment with six optical band-pass filters is disclosed in FIG. 12, many more light waves can be demultiplexed with arrangements of many more filters of different center wavelengths.

FIG. 13 illustrates an example of the demultiplexing characteristics of the demultiplexer 10*d* in FIG. 12. In the figure, the horizontal axis indicates wavelength and the vertical axis shows the insertion loss provided in passing through the optical band-pass filters 11 through 16. Said insertion loss is defined by the following formula;

$$-10 \log \left\{ \frac{\text{(output power from a specified filter)}}{\text{(input power to the demultiplexer)}} \right\}$$

It should be appreciated from FIG. 13 that the light waves of center wavelengths from respective filters are emitted with low loss, but the light waves with wavelengths apart from the center wavelengths are substantially not emitted.

The embodiment illustrated in FIG. 12 is an example of demultiplexer, and it should be appreciated that the same arrangement as that in FIG. 12 can be used as an optical multiplexer which combines a plurality of wavelengths to a single optical fiber.

FIG. 14 shows an embodiment of the present invention used as an optical multiplexer. In the figure, the reference numeral 40' is the rod lens for coupling an optical beam from the transmission optical fiber 100 to the multiplexer; 41', 42', 43', 44', 45' and 46' are rod lenses which collimate output from the optical fibers to parallel beams, 51', 52', 53', 54', 55', 56' are optical fibers which guide light waves to be multiplexed, and those optical fibers 51', 52', 53', 54', 55' and 56' guide the light waves having the wavelengths $\lambda_1, \lambda_2, \lambda_3, \lambda_4, \lambda_5, \lambda_6$, respectively. Those waves are collimated to parallel beams through the rod lenses 41', 42', 43', 44', 45' and 46', respectively, and the collimated beams are applied to the common substrate 60 at an oblique incident angle through optical band-pass filters. Those collimated beams propagate in the opposite direction to that when they propagate in the case of FIG. 12, and the collimated beams enter into the rod lens 40', which couples the multiplexed beams to the transmission optical fiber 100.

As an example, the light wave with wavelength λ_2 guided by the optical fiber 52' is described in the following explanation. The light wave from the optical fiber 52' is collimated to a parallel beam by the collimating rod lens 42' and then is applied to the optical band-pass filter 11 with an oblique incident angle through the prism 82, the optical band-pass filter 12 and the common substrate 60. On the other hand, the light beams of the wavelengths $\lambda_3, \lambda_4, \lambda_5, \lambda_6$ which are applied to the optical band-pass filter 12 from the bottom in FIG. 14 are reflected by the optical band-pass filter 12, and along with the light beam having the wavelength λ_2, those reflected beams enter into the optical band-pass filter 11. Those beams which are applied to the optical band-pass filter 11 are reflected by the optical band-pass filter 11, which also transmits the wavelength λ_1. The output beams from the optical band-pass filter 11 are coupled with the transmission optical fiber 100 through the prism 80, and the rod lens 40'.

FIG. 15 illustrates another embodiment of the present multiplexer/demultiplexer according to the present invention. The same reference numerals are given to the components which have been illustrated in FIG. 12. The important feature of this embodiment is that the demultiplexed beams do not enter an optical fiber, but are applied directly to the light detectors or sensors 71, 72, 73, 74, 75, and 76 through the rod lenses 41, 42, 43, 44, 45, 46.

FIG. 16 illustrates another embodiment of the present multiplexer/demultiplexer according to the present invention. The basic performance of this embodiment in FIG. 16 is the same as that of the embodiments in FIG. 12 and FIG. 14. The important feature of FIG. 16 is that the dielectric thin film filters 11, 12, 13, 14, 15 and 16 having a bandpass property are attached directly to the surface of the prisms 81, 82, 83, 84, 85, 86 or on the surface of the common substrate 60 through a vacuum evaporation or sputtering process. Therefore, no glass plate or glass protection is provided in the embodiment in FIG. 16.

It should be noted as indicated in FIG. 6, that the center wavelength λ_0 of an optical band-pass filter can be adjusted by controlling the angle of incidence of the input light beam. By utilizing this characteristic, when the center wavelength of an optical band-pass filter has some deviation from the desired value because of an error in the manufacturing process, fine adjustment of the center wavelength of a band-pass optical filter is possible.

FIG. 17 illustrates still another embodiment of the present multiplexer/demultiplexer which can perform the fine adjustment of the center wavelength utilizing the above characteristics. The same reference numerals

as those in FIG. 12 are used for those elements in FIG. 17. The important feature of the embodiment in FIG. 17 is the presence of the second group of prisms 91, 92, 93, 94, 95 and 96 for the fine adjustment of the angle of incidence. The vertical angles of these prisms 91, 92, 93, 94, 95 and 96 are designed so that the respective optical band-pass filters 11, 12, 13, 14, 15, 16 shall have optimum angles of incidence. The sum of the vertical angles of the first group of prisms and the second group of prisms is substantially equal to the angle of incidence of a light beam to optical filters. It should be appreciated in the embodiment of FIG. 17, that the diameter of each optical band-pass filter is sufficiently larger than the diameter of an applied optical beam so that an optical beam does not extend beyond an optical filter when an angle of incidence is changed.

In the embodiment in FIG. 17, even if the center wavelengths of the optical band-pass filters 11, 12, 13, 14, 15, and 16 have a small deviation due to the manufacturing error from the desired center wavelengths λ_1, λ_2, λ_3, λ_4, λ_5, λ_6, such errors can be compensated for by adjusting the angle of incidence of an optical beam utilizing compensation prisms 91, 92, 93, 94, 95, and 96. Further, since the diameter of the optical band-pass filters is sufficiently large, the multiplexing and/or demultiplexing operation is not disturbed even when the angle of incidence of an input light beam changes from the designed angle of incidence.

As described above, a multiplexer and/or a demultiplexer according to the present invention has the advantages listed below.

(a) Light beams do not propagate in the air because those elements are optically contacted each other.

(b) Thus, an optical multiplexer/demultiplexer free from external thermal disturbances and mechanical vibrations can be arranged, and its size is readily reducible.

(c) Multiple signal waves can be multiplexed or demultiplexed with small loss by arranging the optical filters in an array.

(d) The signal waves with narrow wavelength spacing can be multiplexed or demultiplexed through the use of the optical band-pass filters.

(e) The characteristics of the device can be adjusted by adjusting the angle of incidence of light beam going into the optical band-pass filters.

(f) Further, without providing an anti-reflection coating on individual components, a low loss multiplexer or demultiplexer whose size is readily reducible can be formed, because the optical fibers, the lenses, the dielectric thin film filters, and the common substrate have the same refractive index.

From the foregoing it will now be apparent that a new and improved optical multiplexer and/or demultiplexer has been found. It should be understood of course that the embodiments disclosed are merely illustrative and are not intended to limit the scope of the invention. Reference should be made to the appended claims, therefore, rather than the specification as indicating the scope of the invention.

Finally the major reference numerals and symbols utilized in the specification are listed below.

1,2,1',2',1",2":	graded index rod lens
3,3',3":	interference film filter
5,6,7:	position
10a,10b,10c,10d,10e,10f,10g,10h:	optical multiplexer/

-continued

MUL, DE-MUL	demultiplexer
11,12,13,14,15,16:	dielectric thin film filter
21,22,23,24,25,26,S_1:	glass plate
31,32,33,34,35,36,S_2:	glass protection
40,41,42,43,44,45,46: 40',41',42',43',44',45',46':	graded index rod lens
51,52,53,54,55,56: 51',52',53',54',55',56':	optical fiber
60;	substrate
60a,60b:	parallel planes of the substrate 60
71,72,73,74,75,76:	light detector
80,81,82,83,84,85,86: 91,92,93,94,95,96:	prism
100,101,102:	optical fiber
111,112,113,114,115:	dielectric thin film filter
121,122,123,124,125: 121',122',123',124',125':	collimating lens
131,132,133,134,135: R_1, R_2, R_n:	light detector
131',132',133',134',135': T_1, T_2, T_n:	light source
140,140':	collimating lens
F_1, F_2:	$\lambda/4$ thin film
F_3:	$\lambda/2$ thin film
λ_1, λ_1', λ_2, λ_2', λ_3, λ_4, λ_5, λ_6:	wavelength

What is claimed is:

1. An optical multiplexer comprising a plurality of flat optical filter means, each of which transmits a different predetermined wavelength and reflect other wavelengths, said optical filter means being arranged substantially in a pair of spaced parallel rows, the filter means in the first row being staggered in relation to the corresponding filter means in the second row so that an optical beam is transmitted or reflected by the optical filter means in sequence; an optical means provided behind each of said optical filter means to provide a parallel optical beam from an optical source to each of said optical filter means with a small angle of incidence, and another optical means provided at the output of the final optical filter means to connect the output optical beam to an optical fiber.

2. An optical multiplexer according to claim 1, wherein said optical filter means is a dielectric thin film filter having a bandpass property.

3. An optical multiplexer according to claim 1, further comprising means for adjusting the angle of incidence of a light beam to the optical filter means to control the center wavelength of each optical filter means, said adjusting means being provided for each optical filter means.

4. An optical demultiplexer comprising a plurality of flat optical filter means each of which transmits a different predetermined wavelength and reflects other wavelengths, said optical filter means being arranged substantially in a pair of spaced parallel rows, the filter means in the first row being staggered in relation to the corresponding filter means in the second row so that an optical beam is transmitted or reflected by said optical filter means in sequence; an optical means for applying a collimated input optical beam to each of said optical filter means with a small angle of incidence; and another optical means confronting each of said optical filter means to receive and focus the transmitted beam from

each optical filter means for illuminating a light detector.

5. An optical demultiplexer according to claim 4, wherein said optical filter means is a dielectric thin film filter having a bandpass property.

6. An optical demultiplexer according to claim 4, further comprising means for adjusting the angle of incidence of a light beam to the optical filter means to control the center wavelength of each optical filter means, said adjusting means being provided for each optical filter means.

7. An optical multiplexer comprising a transparent dielectric substrate having first and second parallel planes, a first group of optical filters positioned linearly on said first plane, a second group of optical filters positioned linearly on the second plane and staggered in relation to the corresponding filters on the first plane, projecting means for projecting collimated optical beams to each of said optical filters at a predetermined angle of incidence, and coupling means provided at the output of the final optical filter to connect the output optical beam to an outside optical fiber, wherein each said optical filter transmits a wave having a different predetermined wavelength and reflects waves having other wavelengths.

8. An optical multiplexer according to claim 7, wherein said projecting means for projecting collimated optical beams to each of the optical filters at a predetermined angle of incidence includes a prism.

9. An optical multiplexer according to claim 7, wherein the angle of incidence is approximate 15°.

10. An optical multiplexer according to claim 7, wherein said optical filters are directly attached to the parallel surfaces of the substrate.

11. An optical multiplexer according to claim 7, wherein all the optical elements provided in the path of the light beam are in optical contact so that the optical beam does not pass through air.

12. An optical multiplexer according to claim 7, wherein all the optical elements provided along the path of the light beam have approximately the same refractive index as each other so that the light beam does not reflect at the contact surface of two elements.

13. An optical multiplexer according to claim 7, further comprising a second prism inserted between the substrate and each optical filter for adjusting the angle of incidence.

14. An optical demultiplexer comprising a transparent dielectric substrate having first and second parallel planes, a first group of optical filters positioned linearly on said first plane, a second group of optical filters positioned linearly on the second plane and staggered in relation to the corresponding filters on the first plane, projecting means for projecting the collimated optical beam to the first optical filter at a predetermined angle of incidence, and at least one light detector provided behind each optical filter, wherein each said optical filter transmits a wave having a different predetermined wavelength and reflects waves having other wavelengths.

15. An optical demultiplexer according to claim 14, wherein said projecting means for projecting the collimated optical beam to the first optical filter at a predetermined angle of incidence includes a prism.

16. An optical demultiplexer according to claim 14, wherein the angle of incidence is approximate 15°.

17. An optical demultiplexer according to claim 14, wherein said optical filters are directly attached to the parallel surface of the substrate.

18. An optical demultiplexer according to claim 14, wherein all the optical elements provided along the path of the light beam are in optical contact so that an optical beam does not pass through air.

19. An optical demultiplexer according to claim 14, wherein all the optical elements provided along the path of the light beam have approximately the same refractive index as each other so that the light beam does not reflect at the contact surface of two elements.

20. An optical demultiplexer according to claim 14, further comprising a second prism inserted between the substrate and each optical filter for adjusting the angle of incidence.

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